

A New Type of Computable Inductor

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The mutual inductance analog of the generalized Thompson-Lampard theorem (for cross capacitances) is developed. An infinitely long cage of five parallel wires can yield an absolute inductance of

$$10^{-7} \ln \frac{3+\sqrt{5}}{2}$$

henries per meter. End-effects of order $1/l^2$ occur in a finite cage, but can be reduced to order $1/l^4$ by using eight wires.

The eight-wire cage has the advantage of overdetermined relations among the inductances to be measured, allowing an estimate of experimental error in the calibration of a standard. Errors due to faulty cage geometry are shown to be of the order of 1 in 10^7 .

The Thompson-Lampard theorem relates to the cross-capacitances of a cylindrical configuration of conductors. Consider a conducting cylindrical shell whose right cross section is an arbitrary closed curve, divided into four segments by infinitesimal gaps. The generalized theorem¹ states that the two cross capacitances, per unit length of the cylinder, are related by

$$e^{-4\pi^2 C_1/\Gamma_e} + e^{-4\pi^2 C_2/\Gamma_e} = 1$$

where Γ_e (often written ϵ_0) is the electric constant of the system of units considered.

The generality of this theorem suggests that an analogous theorem should exist for the mutual inductances of a cage of parallel wires. Consider first an infinitely long cage of four parallel wires, penetrating a transverse plane as in figure 1.



FIGURE 1

Three mutual inductances are involved; the pairs of loops whose traces in the plane are (1) \overline{ab} and \overline{cd} , (2) \overline{ad} and \overline{bc} , (3) \overline{ac} and \overline{bd} . In case (1), the mutual inductance per unit cage length is

$$m = \frac{\Gamma_m}{2\pi} \ln \frac{\overline{ac} \overline{bd}}{\overline{ad} \overline{bc}} \quad (1)$$

where Γ_m is the magnetic constant, often written μ_0 . By considering a, b, c, d to be points in a complex variable plane, we can write

$$m = \frac{\Gamma_m}{2\pi} \ln \left| \frac{(a-c)(b-d)}{(a-d)(b-c)} \right|. \quad (2)$$

¹ D. G. Lampard and R. D. Cutkosky, Some results on the cross capacitances per unit length of cylindrical three-terminal capacitors with thin dielectric films on their electrodes, I.E.E. Monograph 351 M, 1960.

We shall find it convenient to use

$$m = -\frac{\Gamma_m}{2\pi} \ln |x| = -\frac{\Gamma_m}{4\pi} \ln A \quad (3)$$

where A is the square of the absolute value of the cross ratio x .

The desired theorem is a *nonhomogeneous* identity among the several mutual inductances. It can be expressed as an identity among the cross ratios. Thus the problem is to find a geometrical identity among the cross ratios of a set of points in a plane.

Now

$$x_1 \equiv \frac{(a-d)(b-c)}{(a-c)(b-d)} \quad x_2 \equiv \frac{(a-b)(d-c)}{(a-c)(d-b)}$$

yielding the identity

$$x_1 + x_2 \equiv 1. \quad (4)$$

If the four points lie on a circle (including a straight line), the cross ratios are *real* (and positive), so that $|x_1| + |x_2| = 1$, yielding

$$e^{-2\pi m_1/\Gamma_m} + e^{-2\pi m_2/\Gamma_m} = 1 \quad (5)$$

corresponding to the Thompson-Lampard theorem. Unfortunately, departures from a circular locus make the x 's complex, and eq (4) no longer implies any relation between the $|x|$'s.

The third possible pairing corresponds to crossed loops, with

$$x_3 = \frac{(a-b)(c-d)}{(a-d)(c-b)}$$

and is related to the others through

$$x_3 \equiv -x_2/x_1$$

yielding the *homogeneous* identity,

$$m_3 = |m_2 - m_1|$$

which is a circuit relation, independent of the cage configuration:

1. Pentagonal Cage

For a five-wire cage, there are five pairs of sides (fig. 2).

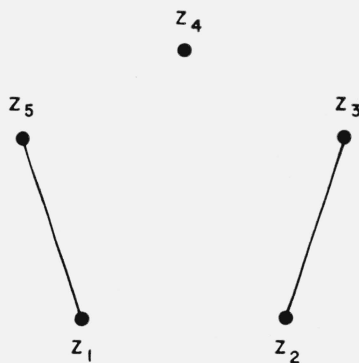


FIGURE 2
(Illustrating loops for M_1).

There are five mutual inductances corresponding to pairs of nonadjacent sides:

$$x_i \equiv \frac{(z_{i+1} - z_i)(z_{i+2} - z_{i-1})}{(z_{i+1} - z_{i-1})(z_{i+2} - z_i)}, \text{ indices modulo } 5$$

There are also five crossed-pairs (fig. 3):

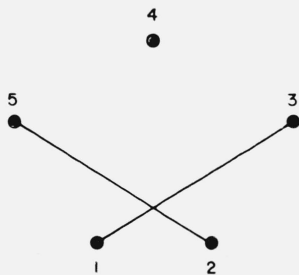


FIGURE 3
(Illustrating loops for N).

$$y_i \equiv \frac{(z_{i+2} - z_{i+1})(z_i - z_{i-1})}{(z_{i+2} - z_{i-1})(z_i - z_{i+1})}$$

related to the x_i through the identity

$$x_i y_i \equiv -x_{i-1} x_{i+1}$$

which yields the circuit relation

$$m_i + n_i = m_{i-1} + m_{i+1}.$$

The five x_i are mutually related by the nonhomogeneous identities

$$x_i + x_{i-1} x_{i+1} \equiv 1. \quad (6)$$

These identities will be shown to yield an identity among $|x_i|$, and therefore among the m_i . The result is the desired analog of the Thompson-Lampard theorem.

2. Derivation of Theorem for Pentagonal Cage

The identities (6) with $i=1$ and $i=2$ can be combined to yield

$$x_3 + x_5 - \frac{1}{x_1} - \frac{1}{x_2} = -\frac{x_1}{x_2} - \frac{x_2}{x_1}. \quad (7)$$

The identities (6) for $i=1, 2, 3, 5$ yield directly

$$\begin{aligned} |1 - x_3|^2 &= |x_2 x_4|^2 = A_2 A_4 \\ |1 - x_5|^2 &= |x_1 x_4|^2 = A_1 A_4 \\ \left|1 - \frac{1}{x_1}\right|^2 &= \left|\frac{x_2 x_5}{x_1}\right|^2 = A_2 A_5 / A_1 \\ \left|1 - \frac{1}{x_2}\right|^2 &= \left|\frac{x_1 x_3}{x_2}\right|^2 = A_1 A_3 / A_2 \end{aligned} \quad (8)$$

where

$$A_i \equiv |x_i|^2.$$

We also have the purely algebraic identity

$$|1-x_3|^2 + |1-x_5|^2 - \left|1-\frac{1}{x_1}\right|^2 - \left|1-\frac{1}{x_2}\right|^2 - |x_3|^2 - |x_5|^2 + \left|\frac{1}{x_1}\right|^2 + \left|\frac{1}{x_2}\right|^2 \equiv -2 \operatorname{Re} \left(x_3 + x_5 - \frac{1}{x_1} - \frac{1}{x_2} \right). \quad (9)$$

Using (7) and (8), this becomes

$$\begin{aligned} A_2 A_4 + A_1 A_5 - A_2 A_5 / A_1 - A_1 A_3 / A_2 - A_3 - A_5 + 1 / A_1 + 1 / A_2 &= 2 \operatorname{Re} \left(\frac{x_1}{x_2} + \frac{x_2}{x_1} \right) \\ &= 2 \operatorname{Re} \left(\frac{x_1 \bar{x}_2}{A_2} + \frac{x_2 \bar{x}_1}{A_1} \right) \\ &= 2(\alpha_1 \alpha_2 + \beta_1 \beta_2) \left(\frac{1}{A_1} + \frac{1}{A_2} \right) \end{aligned} \quad (10)$$

where

$$x_i \equiv \alpha_i + j\beta_i, \quad \bar{x}_i \equiv \alpha_i - j\beta_i.$$

Now identity (6) for $i=1$, $x_1 + x_2 x_5 \equiv 1$

yields

$$\begin{aligned} 2\alpha_1 &= 1 + A_1 - A_2 A_5 \\ \beta_1^2 &\equiv |x_1|^2 - \alpha_1^2 = A_1 - \alpha_1^2. \end{aligned} \quad (11)$$

Solving (10) for $\beta_1 \beta_2$, squaring for $\beta_1^2 \beta_2^2$, and substituting from (11) for β_1^2 , α_1 , and from the similar relations for β_2^2 , α_2 , leads to lengthy algebraic manipulation which yields

$$\begin{aligned} A_1 A_2 A_3 A_4 A_5 - A_1^2 A_3 A_4 - A_2^2 A_4 A_5 - A_3^2 A_5 A_1 - A_4^2 A_1 A_2 - A_5^2 A_2 A_3 \\ + A_1 A_2 A_4 + A_2 A_3 A_5 + A_3 A_4 A_1 + A_4 A_5 A_2 + A_5 A_1 A_3 \\ + A_1 A_3 + A_2 A_4 + A_3 A_5 + A_4 A_1 + A_5 A_2 - A_1 - A_2 - A_3 - A_4 - A_5 + 1 \equiv 0. \end{aligned} \quad (12)$$

Replacing each A_i by $e^{-4\pi m_i / \Gamma_m}$ yields the mutual inductance identity.

If the pentagon is regular, the A_i are equal, and (12) can be factored:

$$(A^2 - 3A + 1)^2 (A + 1) = 0. \quad (13)$$

The allowable roots are

$$A = \frac{3 \pm \sqrt{5}}{2}$$

corresponding to

$$m = \frac{\Gamma_m}{4\pi} \ln \frac{3 + \sqrt{5}}{2}.$$

(The two roots are reciprocal, so yield the same absolute value of mutual inductance.)

3. Application

In principle, we measure the approximately equal m_i by comparison with a standard, m . The assumed value of the standard is in error by an unknown factor $(1+\delta)$. The object of the experiment is to determine δ .

If

$$m_i = a_i m = \frac{a_i}{1+\delta} (1+\delta) m$$

the apparent, or measured values, are

$$\hat{m}_i = \frac{a_i m}{1+\delta} = \frac{m_i}{1+\delta}. \quad (14)$$

Substitution into the theorem (12) yields an implicit equation for δ in terms of the observed \hat{m}_i .

In practice, there will be random measurement errors associated with each \hat{m}_i . These will be treated in a later section. A more serious problem is presented by the fact that we cannot measure the inductance per unit length of an infinite cage, but only the change with the length of a finite cage—i.e., end effects must be considered.

4. End Effects

Consider two loops of length l , the loop planes cutting the transverse plane (fig. 4) in the lines ρ_{i-1} and ρ_{i+1} .

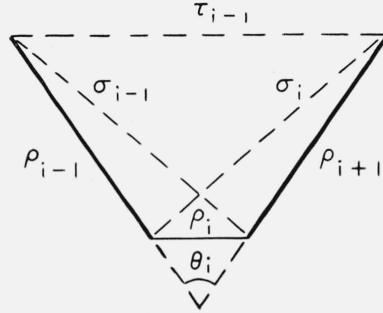


FIGURE 4

The mutual inductance is given by the double line integral around the two loops:

$$M_i = \frac{\Gamma_m}{4\pi} \oint \oint \frac{d\lambda_1 \cdot d\lambda_2}{R_{12}}.$$

End effects arise from the truncation of the cage at length l , and also from the couplings among the shorting bars of length ρ_{i-1} and ρ_{i+1} at the cage ends. The expression for M_i becomes:

$$\begin{aligned} \frac{4\pi M_i}{\Gamma_m} = & \int_0^l \int_0^l dx dy \{ [(x-y)^2 + \rho_i^2]^{-1/2} + [(x-y)^2 + \tau_{i-1}^2]^{-1/2} - [(x-y)^2 + \sigma_{i-1}^2]^{-1/2} \\ & - [(x-y)^2 + \sigma_i^2]^{-1/2} \} + 2 \cos \theta_i \int_0^{\rho_{i-1}} \int_0^{\rho_{i+1}} \left\{ \frac{1}{r} - \frac{1}{\sqrt{l^2 + r^2}} \right\} dudv \quad (15) \end{aligned}$$

where r is the distance in the transverse plane between point u on ρ_{i-1} and point v on ρ_{i+1} .

Since we are considering inductance per unit length, we are interested in

$$m_i = \frac{\Delta M_i}{\Delta l} = \frac{\partial M_i}{\partial l} + \frac{\Delta l}{2} \frac{\partial^2 M_i}{\partial l^2}$$

particularly when l is large compared to the cross dimensions of the cage. We have

$$\begin{aligned} \frac{4\pi}{\Gamma_m} \frac{\partial M_i}{\partial l} = & 2 \int_0^l dx \{ [(l-x)^2 + \rho_i^2]^{-1/2} + [(l-x)^2 + \tau_{i-1}^2]^{-1/2} - [(l-x)^2 + \sigma_{i-1}^2]^{-1/2} \\ & - [(l-x)^2 + \sigma_i^2]^{-1/2} \} + 2l \cos \theta_i \int_0^{\rho_{i-1}} \int_0^{\rho_{i+1}} dudv (l^2 + r^2)^{-3/2} = \ln \frac{\sigma_{i-1}^2 \sigma_i^2}{\tau_{i-1}^2 \rho_i^2} \\ & + 2 \ln \frac{(l + \sqrt{l^2 + \rho_i^2}) (l + \sqrt{l^2 + \tau_{i-1}^2})}{(l + \sqrt{l^2 + \sigma_i^2}) (l + \sqrt{l^2 + \sigma_{i-1}^2})} + 2l \cos \theta_i \int_0^{\rho_{i-1}} \int_0^{\rho_{i+1}} dudv (l^2 + r^2)^{-3/2}. \quad (16) \end{aligned}$$

For large l , this is approximated by

$$\frac{4\pi}{\Gamma_m} \frac{\partial M_i}{\partial l} \doteq \ln \frac{\sigma_{i-1}^2 \sigma_i^2}{\tau_{i-1}^2 \rho_i^2} + \frac{\rho_i^2 + \tau_{i-1}^2 - \sigma_{i-1}^2 - \sigma_i^2}{2l^2} + \frac{2\rho_{i-1}\rho_{i+1} \cos \theta_i}{l^2} - \frac{3}{16l^4} (\rho_i^4 + \tau_{i-1}^4 - \sigma_{i-1}^4 - \sigma_i^4) - \frac{3}{2} \frac{\rho_{i-1}\rho_{i+1} \cos \theta_i}{l^4} \left\{ \tau_{i-1}^2 + \rho_i^2 + \rho_{i-1}\rho_{i+1} \cos \theta_i + \frac{3}{2} (\rho_{i-1}^2 + \rho_{i+1}^2) \right\}. \quad (17)$$

The distances in figure 4 are related by

$$\rho_i^2 + \tau_{i-1}^2 - \sigma_{i-1}^2 - \sigma_i^2 = -2\rho_{i-1}\rho_{i+1} \cos \theta_i$$

simplifying (17) to

$$\frac{4\pi}{\Gamma_m} \frac{\partial M_i}{\partial l} \doteq \ln \frac{\sigma_{i-1}^2 \sigma_i^2}{\tau_{i-1}^2 \rho_i^2} + \frac{\rho_{i-1}\rho_{i+1} \cos \theta_i}{l^2} + \frac{1}{l^4} \left\{ \frac{3}{16} (\rho_i^4 + \tau_{i-1}^4 - \sigma_{i-1}^4 - \sigma_i^4) - \sigma_i^4 + 4\rho_i^2 \tau_{i-1}^2 - 4\sigma_{i-1}^2 \sigma_i^2 - (\rho_{i-1}^2 + \rho_{i+1}^2) \rho_{i-1}\rho_{i+1} \cos \theta_i \right\}. \quad (18)$$

The second derivative, $\partial^2 M_i / \partial l^2$, is easily found and leads to

$$\frac{4\pi}{\Gamma_m} \frac{\Delta M_i}{\Delta l} \doteq \ln \frac{\sigma_{i-1}^2 \sigma_i^2}{\tau_{i-1}^2 \rho_i^2} + \frac{\rho_{i-1}\rho_{i+1} \cos \theta_i}{l^2} \left(1 - \frac{2\Delta l}{l} \right) + \frac{a}{l^4} \left(1 - \frac{4\Delta l}{l} \right) \quad (19)$$

where a stands for the coefficient of $1/l^4$ in eq (18).

For large Δl , integration of (18) yields

$$\frac{4\pi}{\Gamma_m} \frac{M_i(l_2) - M_i(l_1)}{l_2 - l_1} \doteq \ln \frac{\sigma_{i-1}^2 \sigma_i^2}{\tau_{i-1}^2 \rho_i^2} + \frac{\rho_{i-1}\rho_{i+1} \cos \theta_i}{l_1 l_2} + \frac{a}{3} \frac{l_1^2 + l_1 l_2 + l_2^2}{l_1^3 l_2^3}. \quad (19a)$$

For a regular pentagon, $\sigma^2 = \tau^2 = \frac{3+\sqrt{5}}{2} \delta^2$, $\theta = \pi/5$,
yielding

$$\frac{4\pi}{\Gamma_m} \frac{\partial M}{\partial l} \doteq \ln \frac{3+\sqrt{5}}{2} + \frac{1+\sqrt{5}}{4} \rho^2 / l^2. \quad (20)$$

The ρ^2/l^2 end-effect is intolerable. Equation (19) suggests the use of an octagon, $\cos \theta = 0$. For a regular octagon,

$$\sigma^2 = \rho^2(2+\sqrt{2}), \quad \tau^2 = \rho^2(3+2\sqrt{2}) \quad (21)$$

yielding

$$\frac{4\pi}{\Gamma_m} \frac{\partial M}{\partial l} \doteq \ln 2 - 3 \frac{(3+2\sqrt{2})}{8} \rho^4 / l^4 \quad (22)$$

with a tolerable end-effect. Errors due to irregularity of the octagon will be treated later.

5. Octagonal Cage

Since cross ratios are invariant under bilinear transformations, three points of a polygonal cage can be chosen arbitrarily. This implies that there are $2(n-3)$ independent mutual inductances. For the pentagon, $2(n-3)=4$, providing one identity among the five mutual inductances. In the case of an octagon, there are 10 independent mutual inductances, so the 8 pairs of mutually perpendicular sides are insufficient. There are, however, additional pairs of perpendicular loops (fig. 5). Fortunately, the dotted pair and the solid pair have the same nominal value of mutual inductance. Among the 16 mutual inductances now under consideration, there are two circuit identities, leaving 14 essentially independent measurements. This is a sufficient overdetermination of the cross ratios of the cage to yield a reasonable estimate of the validity of the final determination of δ in the presence of random errors of measurement.

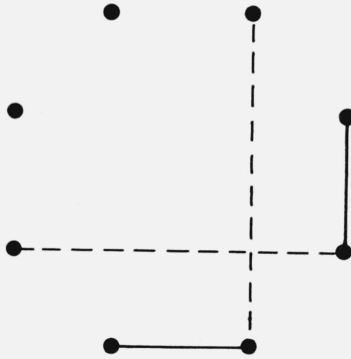


FIGURE 5

For the two sets of mutual inductances per unit length, of an infinite cage, we have

$$m_i = \frac{\Gamma_m}{4\pi} \ln \frac{\sigma_{i-1}^2 \sigma_i^2}{\tau_{i-1}^2 \rho_i^2}$$

$$n_i = \frac{\Gamma_m}{4\pi} \ln \frac{\sigma_{i-2}^2 \sigma_{i+1}^2}{\rho_i^2 \tau_{i+3}^2}, \text{ indices mod } 8. \quad (23)$$

It does not seem feasible to express the geometric identity among the cross ratios explicitly, as was done for the pentagon eq (12). There is, however, a useful procedure for the *application* of the inherent identity, i.e., for the determination of the calibration constant, δ . We attribute all random measurements errors to random variations of the standard, i.e., to variations in δ . This artifice simplifies the problem and at the same time yields a conservative estimate of the reliability of the calibration of the standard inductor.

We modify eq (14) to the form

$$\hat{m}_i = m_i / (1 + \delta_i)$$

$$\hat{n}_i = n_i / (1 + \delta_{i+8}), \quad i = 0 \dots 7 \quad (24)$$

to allow for errors in the 16 inductance determinations. If there were no experimental errors, all δ_i would be equal, and would be overdetermined by the 16 eq (24). A computer program could be developed to assign positions to the cage wires that would make eq (24) compatible, thus yielding both m_i and δ . In the presence of errors, our best estimate of δ arises from assigning cage coordinates to minimize the variance of the resulting δ_i .²

$$\varphi = \frac{1}{16} \sum_0^{15} (\delta_i - \delta)^2$$

$$\varphi_{\min} = s^2 = \overline{\delta_i^2} - \bar{\delta}^2, \quad \delta = \bar{\delta}. \quad (25)$$

Cage coordinates are to be assigned to minimize s^2 . From eq (24), we have

$$s^2 = \frac{1}{16} \sum_0^7 \left(\frac{m_i - \hat{m}_i}{\hat{m}_i} \right)^2 + \frac{1}{16} \sum_0^7 \left(\frac{n_i - \hat{n}_i}{\hat{n}_i} \right)^2 - \left\{ \frac{1}{16} \sum_0^7 \frac{m_i - \hat{m}_i}{\hat{m}_i} + \frac{1}{16} \sum_0^7 \frac{n_i - \hat{n}_i}{\hat{n}_i} \right\}^2. \quad (26)$$

² This procedure was suggested by Dr. R. J. Arms.

The theoretical values m_i , n_i , are computed from assigned cage coordinates using eq (23). Since the m_i and n_i depend only upon cross ratios, and cross ratios are unaffected by bilinear transformations, three of the cage points can be arbitrarily assigned. The other five are then adjusted to minimize s^2 . When s^2 is minimized, the term in braces in (26) is the desired value of δ . The measured values \hat{m}_i and \hat{n}_i will be essentially equal, so this term can be approximated by

$$\delta \doteq \frac{\Sigma m_i + \Sigma n_i}{\Sigma \hat{m}_i + \Sigma \hat{n}_i} - 1. \quad (27)$$

For displacement of cage wires from the vertices of a regular octagon, both Σm_i and Σn_i are at a saddle point. In fact, for displacement of any one wire in a direction making an angle φ with the radius from the octagon center, we have

$$\frac{\partial \sum_i m_i}{\partial (r/\rho)} = \frac{\partial \sum_i n_i}{\partial (r/\rho)} = 0 \quad (28a)$$

$$\frac{\partial^2 \sum_i m_i}{\partial (r/\rho)^2} = \frac{\partial^2 \sum_i n_i}{\partial^2 (r/\rho)^2} = -\frac{\Gamma_m}{\pi} (2 - \sqrt{2}) \cos 2\varphi. \quad (28b)$$

Thus an ignored displacement of one wire from its regular position would affect s^2 , but not δ , to first order. The second order effect on δ vanishes if averaged over all directions of displacement.

6. End Effects

The use of a regular octagon reduces end effects to terms in $1/l^4$. Departures from regularity introduce end effects in $1/l^2$. Formulas (18) and (19) in M_i are converted to the corresponding formulas in N_i by the following changes:

$$\begin{array}{lll} \sigma_{i-1} \rightarrow \sigma_{i-2} & \rho_i \rightarrow \rho_i & \theta_i \rightarrow \varphi_i \\ \sigma_i \rightarrow \sigma_{i+1} & \rho_{i-1} \rightarrow \tau_{i-2} & \\ \tau_{i-1} \rightarrow \tau_{i+3} & \rho_{i+1} \rightarrow \tau_i & \end{array}$$

where φ_i is the angle between τ_{i-2} and τ_i (fig. 6).

The computed m_i and n_i used for minimizing s^2 eq (26) can be taken from eq (19) and its n_i equivalent, thus automatically allowing for end effects. Ignoring these end effects by using the infinite-cage formula in the minimization would still produce only a small error.

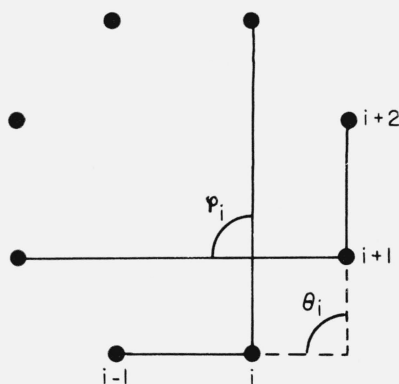


FIGURE 6

For a regular octagon, eq (21) yields a fractional error of

$$-\frac{3(3+2\sqrt{2})}{8 \ln 2} \rho^4/l^4$$

in m_i , and the corresponding formula for n_i yields a fractional error of

$$-\frac{3(3+2\sqrt{2})^3}{8 \ln 2} \rho^4/l^4.$$

The resulting fractional error in $\Sigma(m_i+n_i)$ is approximately $-7\rho^4/l^4$, which is of the order of 10^{-7} for $\rho/l=0.01$.

We must also investigate the error arising from the $1/l^2$ term for a slightly irregular octagon. For the m_i , we have

$$\epsilon_i = \rho_{i-1} \rho_{i+1} \cos \theta_i / l^2 \ln 2$$

and for the n_i , $\epsilon_i = \tau_{i-2} \tau_i \cos \phi_i / l^2 \ln 2$. By eq (27), these terms lead to an erroneous δ , or fractional error in the mutual inductance assigned to the standard, equal to $\bar{\epsilon}_i$:

$$\delta_e = \frac{\Sigma \epsilon_i}{16} = \frac{\Sigma (\rho_{i-1} \cdot \rho_{i+1} + \tau_{i-2} \cdot \tau_i)}{16 l^2 \ln 2}.$$

If points 1, 2, 3 are fixed, and the other five displaced from nominal by η_i , we find

$$\Sigma \epsilon_i = \frac{2}{l^2 \ln 2} [2\eta_5 \cdot \eta_7 + 2\eta_6 \cdot \eta_8 + \eta_4 \cdot \eta_6 - \eta_4 \cdot \eta_5 - \eta_4 \cdot \eta_7 - \eta_5 \cdot \eta_6 - \eta_5 \cdot \eta_8 - \eta_6 \cdot \eta_7 - \eta_7 \cdot \eta_8].$$

If

$$|\eta| \leq \alpha, \text{ then } |\Sigma \epsilon_i| \leq \frac{2}{l^2 \ln 2} 11\alpha^2$$

and

$$|\delta_e| \leq 2\alpha^2/l^2.$$

For

$$\alpha \sim 0.02\rho \text{ and } \rho \sim 0.01l, |\delta_e| \leq 10^{-7}.$$

7. Other Errors

A bent wire, with zero average displacement, is expected to yield an error similar to that of an ignored displacement, but of lower order. An ignored displacement affects $s^2(\delta)$ but not $\bar{\delta}$. This would have more effect on the reliability of calibration than on the calibration constant itself. Exact analysis of the bent wire situation is difficult; the effect should be checked experimentally by adding known perturbations to the cage.

The analysis has assumed ideal wires. Actual construction requires finite diameters. It is well known (and easily shown) that at zero frequency, such wires are equivalent to ideal wires. Proximity effects on the current distribution can be experimentally lumped with skin effect, and the net effect evaluated by making measurements at various frequencies. Non-geometrical effects, such as produced by the permeability of the wire and supports, will be investigated in the future.

8. Conclusion

It has been shown that there is a mutual inductance analog of the Thompson-Lampard theorem. In particular, a design is proposed wherein end effects are substantially reduced. The mutual inductance of this design is $\ln 2/10 \mu\text{h/m}$.

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